## High-Altitude <br> Balloon <br> Atmospheric Database

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## Presentation Outline

- Introduction
- Purpose and Use of This Database
- Notes and Future Work
- Conclusion
- Acknowledgements


## Introduction

- A Few Uses of High Altitude Balloons
- Satellite Sensor Testing
- Student Experiments
- Importance of Balloon Retrieval
- Guessing Gas Amount
- Helium Shortage*
- Potential Waste of Both Time and Money
- Database Information
- Tolex Balloons from Kaymont Consolidated Industries
- Helium and Hydrogen Tanks Rented from Indiana Oxygen
- Currently a Microsoft Excel Workbook
*"Dwindling Stockpile of Helium Causes Concerns by Brad Palmer from The Washington Post, Published May 12, 2012 , Accessed June 15, 2012 from The Washington Post website.


## Purpose

- Provide Useful Atmospheric Properties
- Provide Balloon Properties
- Assist in the Estimation of Maximum Balloon Altitude
- Provide Multiple Charts and Graphs for the use in Analyzing Balloon and Atmospheric Properties


## Database: Atmospheric Properties

- Speed of Sound
- Dynamic Viscosity
- Kinematic Viscosity
- Mean Air

Particle Speed

- Mean Collision Frequency
- Mean Free Path
- Mole Volume

| 2 Allitude |  | Temp atmo. | Speed of Sound | Dynamic Viscosity | Kinematic Viscosity | Mean Air Particle Speed | Mean Collision frequency | Mean free Path | Mole Volume |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 (km) |  | (K) | (mis) | (11s $\mathrm{m}^{2}$ ) | (m²) | (ms) | Hz (11s) | (m) | $\mathrm{m}^{\text {2 }}$ kmol |
| 4 | 0 | 288.15 | 340.294 | 1.7894E-05 | 1.4607E-05 | 459.945 | $6.9189 E+09$ | 6.6332E-08 | 23.64 |
| 5 | 1 | 281.65 | 336.435 | 1.7579E-05 | 1.5813E-05 | 453.740 | 6.2070 E+09 | 7.3095E-08 | 26.06 |
| 6 | 2 | 275.15 | 332.532 | 1.7260E-05 | 1.7147E-05 | 448.476 | $5.5554 E+09$ | 8.0728E-08 | 28.78 |
| 7 | 3 | 268.66 | 328.584 | 1.6938E-05 | 1.8626E-05 | 443.151 | $4.9588 \mathrm{E}+09$ | 8.9367E-08 | 31.86 |
| 8 | 4 | 262.17 | 324.599 | 1.6612E-05 | 2.02755-05 | 437.763 | 4.4141E+09 | 9.9173E-08 | 35.35 |
| 9 | 5 | 255.68 | 320.545 | 1.6282E-05 | 2.2110E-05 | 432.310 | $3.9180 E+09$ | 1.1034E-07 | 39.33 |
| 10 | 6 | 249.19 | 316.452 | 1.5949E-05 | 2.4162--05 | 426.789 | 3.4671 E+09 | 1.2310E-07 | 43.88 |
| 11 | 7 | 242.70 | 312.306 | 1.5612E-05 | 2.6461E.05 | 421.198 | $3.0584 E+09$ | $1.3772 E^{-07}$ | 49.09 |
| 12 | 8 | 236.22 | 308.105 | 1.5271E-05 | 2.9044--05 | 415.533 | $2.6888 \mathrm{E}+09$ | 1.5454E-07 | 55.09 |
| 13 | 9 | 229.73 | 303.848 | 1.4926E-05 | 3.1957E-05 | 409.791 | 2.3555E+09 | 1.7397E-07 | 62.01 |
| 14 | 10 | 223.25 | 299.532 | 1.4577E-05 | 3.5251E.05 | 403.970 | $2.0558 E+09$ | 1.9651E-07 | 70.05 |
| 15 | 11 | 216.77 | 295.154 | 1.4223E-05 | 3.8988E-05 | 398.065 | 1.7871 E+09 | 2.2274E-07 | 79.40 |
| 16 | 12 | 216.65 | 295.070 | 1.4216E-05 | 4.5574E-05 | 397.952 | $1.5277 E+09$ | 2.6049E-07 | 92.85 |
| 17 | 13 | 216.65 | 295.070 | 1.4216E-05 | 5.3325-05 | 397.952 | $1.3056 E+09$ | 3.049E-07 | 108.65 |
| 18 | 14 | 216.65 | 295.070 | 1.4216E-05 | 6.2391E-05 | 397.952 | $1.1159 E+09$ | 3.5662E-07 | 127.12 |
| 19 | 15 | 216.65 | 295.070 | 1.4216E-05 | 7.2995E-05 | 397.952 | $9.5380 \mathrm{E}+08$ | 4.1723E-07 | 148.72 |
| 20 | 16 | 216.65 | 295.070 | 1.4216E-05 | 8.5397E-05 | 397.952 | $8.1528 \mathrm{E}+08$ | 4.8812E-07 | 173.99 |
| 21 | 17 | 216.65 | 295.070 | 1.4216E-05 | 9.99022-05 | 397.952 | 6.9691 E+08 | 5.7102E-07 | 203.54 |
| 22 | 18 | 216.65 | 295.070 | 1.4216E-05 | 1.1686E-04 | 397.952 | $5.9576 E+08$ | 6.6797E-07 | 238.10 |
| 23 | 19 | 216.65 | 295.070 | 1.4216E-05 | 1.3670E-04 | 397.952 | $5.0931 \mathrm{E}+08$ | 7.8135E-07 | 278.52 |
| 24 | 20 | 216.65 | 295.070 | 1.4216E-05 | 1.5989E-04 | 397.952 | $4.3543 E+08$ | $9.1393 E-07$ | 325.77 |
| 25 | 21 | 217.58 | 295.70 | 1.4267E-05 | 1.8843E-04 | 398.806 | $3.7160 E+08$ | 1.0732E-06 | 382.55 |
| 26 | 22 | 218.57 | 296.377 | 1.4322E-05 | 2.2201E-04 | 399.715 | $3.1733 E+08$ | 1.2596E-06 | 448.99 |
| 27 | 23 | 219.57 | 297.049 | 1.4376E-05 | 2.6135E-04 | 400.622 | $2.7119 E+08$ | 1.4772E-06 | 526.57 |
| 28 | 24 | 220.56 | 297.720 | 1.4430E-05 | 3.0743E-04 | 401.526 | 2.3194E+08 | 1.7312E-06 | 617.08 |
| 29 | 25 | 221.55 | 298.389 | 1.4484E-05 | 3.6135E-04 | 402.429 | $1.9852 \mathrm{E}+08$ | 2.0272E-06 | 722.60 |
| 30 | 26 | 222.54 | 299.056 | 1.4538E-05 | 4.2439E-04 | 403.329 | 1.7004E+08 | 2.3720E-06 | 845.51 |
| 1415 | Useful Data | Ascent calc | Culations (Rec. Fill) A | Ascent Dita Table (Rec | c. Fill) Ascent Chats | (ts Rec. Fill) Ascent Calc. | (non-14 | III |  |

Listed atmospheric properties are from an online atmospheric properties calculator ${ }^{3}$ based on the U.S. Standard Atmosphere $1976{ }^{4}$.

## Database: Balloon Properties

- Volume and Diameter
- Coefficient of Drag
- Drag Force
- Free Lift and Lifting Force
- Velocity
- Conductive Heat Transfer
${ }^{-}$See Paper for Nomenclature, Equations, and Derivations used in database


## Database: Recommended Fill <br> - Ascent Calculations (Rec. Fill) Worksheet



## Database: Recommended Fill

- Ascent Data Table (Rec. Fill) Worksheet

| 4 | C | D | E | F | G | H | 1 | J | K | L | M | N | 0 | P | Q | R |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Time ( He ) | Time ( $\mathrm{H}_{2}$ ) | Temp atmo. | Temp atmo. | Temp gas | Temp gas | $\Delta \mathrm{T}(\mathrm{T} \mathrm{T}-\mathrm{Tg})$ | Pressure | Pressure | $\rho$ of air | Vb | Dia. of bal. | Surface Area | Cross. Sec. Area | C. S. Area/rad. | Conductive Heat Trans ${ }^{\text {c }}$ |
| 2 | Sec. (s) | $\mathrm{Sec} .(\mathrm{s})$ | (K) | $\left({ }^{\circ} \mathrm{C}\right)$ | (K) | ( ${ }^{\circ} \mathrm{C}$ ) | (K, ${ }^{\circ} \mathrm{C}$ ) | (atm) | (Psi) | (kg/m) | (m) | (m) | $\left(\mathrm{m}^{2}\right)$ | $\left(\mathrm{m}^{2}\right)$ | (m) | ( $\mathrm{J} / \mathrm{s}$ ) He |
| 3 | 0 | 0 | 288.15 | 15.00 | 286.15 | 13.00 | 2.0 | 1.000 | 14.696 | 1.225 | 1.57 | 1.44 | 6.54 | 1.63 | 2.27 | 0.68 |
| 4 | 177 | 167 | 281.65 | 8.50 | 279.65 | 6.50 | 2.0 | 0.887 | 13.036 | 1.112 | 1.73 | 1.49 | 6.97 | 1.74 | 2.34 | 0.70 |
| 5 | 354 | 333 | 275.15 | 2.00 | 273.15 | 0.00 | 2.0 | 0.785 | 11.531 | 1.007 | 1.91 | 1.54 | 7.45 | 1.86 | 2.42 | 0.73 |
| 6 | 530 | 500 | 268.66 | -4.49 | 266.66 | -6.49 | 2.0 | 0.692 | 10.171 | 0.909 | 2.12 | 1.59 | 7.97 | 1.99 | 2.50 | 0.75 |
| 7 | 707 | 667 | 262.17 | -10.98 | 260.17 | -12.98 | 2.0 | 0.609 | 8.944 | 0.819 | 2.35 | 1.65 | 8.54 | 2.14 | 2.59 | 0.78 |
| 8 | 884 | 833 | 255.68 | -17.47 | 253.68 | -19.47 | 2.0 | 0.533 | 7.840 | 0.736 | 2.61 | 1.71 | 9.17 | 2.29 | 2.68 | 0.81 |
| 9 | 1061 | 1000 | 249.19 | -23.96 | 246.19 | -26.96 | 3.0 | 0.466 | 6.850 | 0.660 | 2.90 | 1.77 | 9.84 | 2.46 | 2.78 | 1.25 |
| 10 | 1237 | 1166 | 242.70 | -30.45 | 238.70 | -34.45 | 4.0 | 0.406 | 5.963 | 0.590 | 3.23 | 1.83 | 10.57 | 2.64 | 2.88 | 1.73 |
| 11 | 1414 | 1332 | 236.22 | -36.93 | 231.22 | -41.93 | 5.0 | 0.352 | 5.172 | 0.526 | 3.61 | 1.90 | 11.38 | 2.84 | 2.99 | 2.24 |
| 12 | 1590 | 1498 | 229.73 | -43.42 | 223.73 | -49.42 | 6.0 | 0.304 | 4.469 | 0.467 | 4.04 | 1.98 | 12.27 | 3.07 | 3.10 | 2.79 |
| 13 | 1767 | 1664 | 223.25 | -49.90 | 216.25 | -56.90 | 7.0 | 0.262 | 3.845 | 0.414 | 4.54 | 2.05 | 13.26 | 3.32 | 3.23 | 3.39 |
| 14 | 1943 | 1829 | 216.77 | -56.38 | 208.77 | -64.38 | 8.0 | 0.224 | 3.294 | 0.365 | 5.12 | 2.14 | 14.36 | 3.59 | 3.36 | 4.03 |
| 15 | 2119 | 1994 | 216.65 | -56.50 | 207.65 | -65.50 | 9.0 | 0.191 | 3.250 | 0.312 | 5.96 | 2.25 | 15.89 | 3.97 | 3.53 | 4.77 |
| 16 | 2295 | 2160 | 216.65 | -56.50 | 206.65 | -66.50 | 10.0 | 0.164 | 2.406 | 0.267 | 6.94 | 2.37 | 17.59 | 4.40 | 3.72 | 5.57 |
| 17 | 2471 | 2325 | 216.65 | -56.50 | 205.65 | -67.50 | 11.0 | 0.140 | 2.056 | 0.228 | 8.08 | 2.49 | 19.47 | 4.87 | 3.91 | 6.45 |
| 18 | 2646 | 2489 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.120 | 1.758 | 0.195 | 9.40 | 2.62 | 21.54 | 5.39: | 4.11 | 7.40 |
| 19 | 2822 | 2654 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.102 | 1.503 | 0.166 | 11.00 | 2.76 | 23.92 | 5.98 | 4.33 | 7.80 |
| 20 | 2998 | 2819 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.087 | 1.284 | 0.142 | 12.87 | 2.91 | 26.56 | 6.64 | 4.57 | 8.22 |
| 21 | 3174 | 2983 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.075 | 1.098 | 0.122 | 15.05 | 3.06 | 29.48 | 7.37 | 4.81 | 8.66 |
| 22 | 3349 | 3148 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.064 | 0.939 | 0.104 | 17.61 | 3.23 | 32.73 | 8.18 | 5.07 | 9.13 |
| 23 | 3525 | 3313 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.055 | 0.803 | 0.089 | 20.59 | 3.40 | 36.33 | 9.08 | 5.34 | 9.62 |
| 24 | 3701 | 3478 | 217.58 | -55.57 | 205.58 | -67.57 | 12.0 | 0.047 | 0.686 | 0.076 | 24.19 | 3.59 | 40.45 | 10.11 | 5.64 | 10.15 |
| 25 | 3877 | 3642 | 218.57 | -54.58 | 206.57 | -66.58 | 12.0 | 0.040 | 0.588 | 0.065 | 28.40 | 3.79 | 45.01 | 11.25 | 5.95 | 10.70 |
| 26 | 4052 | 3807 | 219.57 | -53.58 | 207.57 | -65.58 | 12.0 | 0.034 | 0.503 | 0.055 | 33.32 | 3.99 | 50.07 | 12.52 | 6.27 | 11.29 |
| 27 | 4228 | 3972 | 220.56 | -52.59 | 208.56 | -64.59 | 12.0 | 0.029 | 0.431 | 0.047 | 39.05 | 4.21 | 55.66 | 13.92 | 6.61 | 11.90 |
| 28 | 4404 | 4137 | 221.55 | -51.60 | 209.55 | -63.60 | 12.0 | 0.025 | 0.370 | 0.040 | 45.74 | 4.44 | 61.85 | 15.46 | 6.97 | 12.55 |
| 29 | 4580 | 4302 | 222.54 | -50.61 | 210.54 | -62.61 | 12.0 | 0.022 | 0.318 | 0.034 | 53.53 | 4.68 | 68.69 | 17.17 | 7.35 | 13.22 |
| 30 | 4755 | 4466 | 223.54 | -49.61 | 211.54 | -61.61 | 12.0 | 0.019 | 0.273 | 0.029 | 62.61 | 4.93 | 76.25 | 19.06 | 7.74 | 13.93 |
| 14 | 1-M Asc | cent Data Ta | able (Rec. Fill) | Ascent Cha | rts (Rec. Fill) | Ascent | Calc. (non-Rec | c. Fill $/$ As | scent Data Ta | ab (non-Rec | c. Fill) | 1 | II |  |  | - |

## Database: Recommended Fill

- Ascent Charts (Rec. Fill) Worksheet



## Database: Non-Recommended Fill

- Ascent Calc. (non-Rec. Fill)

Worksheet

- Input Number of Tanks of Gas Including Partial Tanks
- Helium Tank Volume: $291 \mathrm{ft}^{3}$
- Hydrogen Tank Volume: 191 ft ${ }^{3}$
- Approximate moles computed from Ideal Gas law



## Database: Non-Recommended Fill

- Ascent Data Table (non-Rec. Fill) Worksheet

| 4 | E | F | G | H | I | J | K | L | M | N | 0 | P | Q | R | S | T |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Temp atmo. | Temp atmo. | Temp gas | Temp gas | $\Delta \mathrm{T}(\mathrm{Ta}-\mathrm{Tg})$ | Pressure | Pressure | Gas Pressure | Gas Pressure | $\rho$ of air | Vb | Vb | Dia. of bal. | Dia. of bal. | Cross Sec. Area | Cross Sec. Area | Con |
| 2 | (K) | $\left({ }^{\circ} \mathrm{C}\right.$ ) | (K) | $\left({ }^{\circ} \mathrm{C}\right)$ | ( $\mathrm{K}^{\circ} \mathrm{C}$ ) | (atm) | (Psi) | He atm | $\mathrm{H}_{2} \mathrm{~atm}$ | (kg/m) | He ( $\mathrm{m}^{3}$ ) | $\mathrm{H}_{2}\left(\mathrm{~m}^{3}\right)$ | He (m) | $\mathrm{H}_{2}(\mathrm{~m})$ | $\mathrm{He}\left(\mathrm{m}^{2}\right)$ | $\mathrm{H}_{2}\left(\mathrm{~m}^{2}\right)$ | (J/s) |
| 3 | 288.15 | 15.00 | 286.15 | 13.00 | 2.0 | 1.000 | 14.696 | 1.000 | 1.524 | 1.225 | 8.64 | 5.67 | 2.55 | 2.21 | 5.09 | 3.84 |  |
| 4 | 281.65 | 8.50 | 279.65 | 6.50 | 2.0 | 0.887 | 13.036 | 0.887 | 1.351 | 1.112 | 9.52 | 6.25 | 2.63 | 2.28 | 5.43 | 4.10 |  |
| 5 | 275.15 | 2.00 | 273.15 | 0.00 | 2.0 | 0.785 | 11.531 | 0.785 | 1.195 | 1.007 | 10.51 | 6.90 | 2.72 | 2.36 | 5.80 | 4.38 |  |
| 6 | 268.66 | -4.49 | 266.66 | -6.49 | 2.0 | 0.692 | 10.171 | 0.692 | 1.054 | 0.909 | 11.63 | 7.63 | 2.81 | 2.44 | 6.21 | 4.69 |  |
| 7 | 262.17 | -10.98 | 260.17 | -12.98 | 2.0 | 0.609 | 8.944 | 0.609 | 0.927 | 0.819 | 12.90 | 8.47 | 2.91 | 2.53 | 6.65 | 5.02 |  |
| 8 | 255.68 | -17.47 | 253.68 | -19.47 | 2.0 | 0.533 | 7.840 | 0.533 | 0.813 | 0.736 | 14.35 | 9.42 | 3.02 | 2.62 | 7.14 | 5.39 |  |
| 9 | 249.19 | -23.96 | 246.19 | -26.96 | 3.0 | 0.466 | 6.850 | 0.466 | 0.710 | 0.660 | 15.95 | 10.47 | 3.12 | 2.71 | 7.66 | 5.78 |  |
| 10 | 242.70 | -30.45 | 238.70 | -34.45 | 4.0 | 0.406 | 5.963 | 0.406 | 0.618 | 0.590 | 17.76 | 11.66 | 3.24 | 2.81 | 8.23 | 6.22 |  |
| 11 | 236.22 | -36.93 | 231.22 | -41.93 | 5.0 | 0.352 | 5.172 | 0.352 | 0.536 | 0.526 | 19.83 | 13.02 | 3.36 | 2.92 | 8.86 | 6.69 |  |
| 12 | 229.73 | -43.42 | 223.73 | -49.42 | 6.0 | 0.304 | 4.469 | 0.304 | 0.463 | 0.467 | 22.22 | 14.58 | 3.49 | 3.03 | 9.55 | 7.22 |  |
| 13 | 223.25 | -49.90 | 216.25 | -56.90 | 7.0 | 0.262 | 3.845 | 0.262 | 0.398 | 0.414 | 24.96 | 16.38 | 3.63 | 3.15 | 10.33 | 7.80 |  |
| 14 | 216.77 | -56.38 | 208.77 | -64.38 | 8.0 | 0.224 | 3.294 | 0.224 | 0.341 | 0.365 | 28.13 | 18.46 | 3.77 | 3.28 | 11.18 | 8.45 |  |
| 15 | 216.65 | -56.50 | 207.65 | -65.50 | 9.0 | 0.191 | 3.250 | 0.191 | 0.292 | 0.312 | 32.74 | 21.49 | 3.97 | 3.45 | 12.37 | 9.34 |  |
| 16 | 216.65 | -56.50 | 206.65 | -66.50 | 10.0 | 0.164 | 2.406 | 0.164 | 0.249 | 0.267 | 38.12 | 25.02 | 4.18 | 3.63 | 13.69 | 10.34 |  |
| 17 | 216.65 | -56.50 | 205.65 | -67.50 | 11.0 | 0.140 | 2.056 | 0.140 | 0.213 | 0.228 | 44.38 | 29.13 | 4.39 | 3.82 | 15.16 | 11.45 |  |
| 18 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.120 | 1.758 | 0.120 | 0.182 | 0.195 | 51.68 | 33.92 | 4.62 | 4.02 | 16.77 | 12.67 |  |
| 19 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.102 | 1.503 | 0.102 | 0.156 | 0.166 | 60.46 | 39.68 | 4.87 | 4.23 | 18.62 | 14.07 |  |
| 20 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.087 | 1.284 | 0.087 | 0.133 | 0.142 | 70.72 | 46.42 | 5.13 | 4.46 | 20.68 | 15.62 |  |
| 21 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.075 | 1.098 | 0.075 | 0.114 | 0.122 | 82.73 | 54.30 | 5.41 | 4.70 | 22.95 | 17.34 |  |
| 22 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.064 | 0.939 | 0.064 | 0.097 | 0.104 | 96.77 | 63.52 | 5.70 | 4.95 | 25.48 | 19.25 |  |
| 23 | 216.65 | -56.50 | 204.65 | -68.50 | 12.0 | 0.055 | 0.803 | 0.055 | 0.083 | 0.089 | 113.19 | 74.30 | 6.00 | 5.22 | 28.29 | 21.37 |  |
| 24 | 217.58 | -55.57 | 205.58 | -67.57 | 12.0 | 0.047 | 0.686 | 0.047 | 0.071 | 0.076 | 132.95 | 87.27 | 6.33 | 5.50 | 31.49 | 23.79 |  |
| 25 | 218.57 | -54.58 | 206.57 | -66.58 | 12.0 | 0.040 | 0.588 | 0.040 | 0.061 | 0.065 | 156.09 | 102.45 | 6.68 | 5.81 | 35.05 | 26.47 |  |
| 26 | 219.57 | -53.58 | 207.57 | -65.58 | 12.0 | 0.034 | 0.503 | 0.034 | 0.052 | 0.055 | 183.11 | 120.19 | 7.05 | 6.12 | 38.98 | 29.44 |  |
| 27 | 270.56 | -52 59 | 20856 | -64 59 | 12 n | 0 ก29 | - 4.31 | $\cap \mathrm{n} 29$ | ก04.5 |  | 21463 | 14088 | 74.3 | 646 | 43.34 | . 2273 |  |
| 14. | - M Asc | cent Data Table | (Rec. Fill) | Ascent Ch | Charts (Rec. Fill) | All) Ascen | nt Calc. (non- | Rec. Fill) Asc | cent Data Tab ( | (non-Rec. Fill) | 价 1 |  | 111 |  | , |  | -11 |

## Database: Non-Recommended Fill

- Ascent Charts (non-Rec. Fill) Worksheet



## Database: Descent with Small Balloon

- Descent Calculations (SB) Worksheet
- Why a small balloon?
- Balloon size options
- Recommended fill used


Note: Photo credited to reference 4 when the correct reference is 6 .

## Database：Descent with Small Balloon

## －Descent Data Table（SB）Worksheet

| 4 | $J$ | K | L | M | N | 0 | P | Q | R | S | T | U | V | W | X | Y |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Pressure | Pressure | Gas Pressure | $\rho$ of air | Vb | Dia．of bal． | pHe in balloon | pH2 in balloon | v | V | Coef．of Drag | Gravity | Free Lift | Free Lift | Lifting Force | Lifting Force | Mag．Drag F |
| 2 | （atm） | （Psi） | （atm） | $\left(\mathrm{kg} / \mathrm{m}^{2}\right)$ | $\left(\mathrm{m}^{2}\right)$ | （m） | （ $\mathrm{kg} / \mathrm{m}^{2}$ ） | $\left(\mathrm{kg} / \mathrm{m}^{2}\right)$ | （ He ）（m／s） | $\left(\mathrm{H}_{2}(\mathrm{~m} / \mathrm{s})\right.$ | Cd | $\left(\mathrm{m} / \mathrm{s}^{2}\right)$ | He（kg） | $\mathrm{H}_{2}(\mathrm{~kg})$ | （He）（N） | $\left(\mathrm{H}_{2}\right)(\mathrm{N})$ | （He）（N） |
| 3 | 0.003 | 0.042 | 0.003 | 0.004 | 13.74 | Balloon will burst if used w／rec．fill | 0.0006 | 0.0003 | －7．83 | －7．79 | 5.397 | 9.684 | 0.047 | 0.051 | 0.455 | 0.493 |  |
| 4 | 0.003 | 0.048 | 0.003 | 0.005 | 11.22 | Balloon will burst if used w／rec．fill | 0.0007 | 0.0004 | －7．83 | －7．80 | 5.331 | 9.687 | 0.044 | 0.048 | 0.426 | 0.464 |  |
| 5 | 0.004 | 0.055 | 0.004 | 0.005 | 10.22 | Balloon will burst if used w／rec．fill | 0.0008 | 0.0004 | －7．83 | －7．80 | 4.889 | 9.690 | 0.047 | 0.051 | 0.454 | 0.493 |  |
| 6 | 0.004 | 0.063 | 0.004 | 0.006 | 8.79 | Balloon will burst if used w／rec．fill | 0.0009 | 0.0005 | －7．84 | －7．81 | 4.649 | 9.694 | 0.047 | 0.051 | 0.454 | 0.492 |  |
| 7 | 0.005 | 0.072 | 0.005 | 0.007 | 7.55 | Balloon will burst if used w／rec．fill | 0.0011 | 0.0005 | －7．84 | －7．81 | 4.418 | 9.697 | 0.047 | 0.051 | 0.454 | 0.492 |  |
| 8 | 0.006 | 0.083 | 0.006 | 0.008 | 6.47 | Balloon will burst if used w／rec．fill | 0.0012 | 0.0006 | －7．84 | －7．82 | 4.195 | 9.700 | 0.047 | 0.051 | 0.454 | 0.492 |  |
| 9 | 0.007 | 0.096 | 0.007 | 0.010 | 5.53 | Balloon will burst if used w／rec．fill | 0.0014 | 0.0007 | －7．85 | －7．82 | 3.982 | 9.703 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 10 | 0.008 | 0.111 | 0.008 | 0.012 | 4.72 | Balloon will burst if used w／rec．fill | 0.0017 | 0.0008 | －7．85 | －7．83 | 3.777 | 9.706 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 11 | 0.009 | 0.129 | 0.010 | 0.014 | 4.03 | Balloon will burst if used w／rec．fill | 0.0020 | 0.0010 | －7．85 | －7．83 | 3.582 | 9.709 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 12 | 0.010 | 0.150 | 0.011 | 0.016 | 3.46 | Balloon will burst if used w／rec．fill | 0.0023 | 0.0012 | －7．85 | －7．83 | 3.404 | 9.712 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 13 | 0.012 | 0.174 | 0.013 | 0.018 | 2.97 | Balloon will burst if used w／rec．fill | 0.0027 | 0.0014 | －7．85 | －7．83 | 3.235 | 9.715 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 14 | 0.014 | 0.202 | 0.015 | 0.021 | 2.54 | Balloon will burst if used w／rec．fill | 0.0031 | 0.0016 | －7．85 | －7．84 | 3.073 | 9.718 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 15 | 0.016 | 0.235 | 0.018 | 0.025 | 2.18 | Balloon will burst if used w／rec．fill | 0.0037 | 0.0018 | －7．86 | －7．84 | 2.918 | 9.721 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 16 | 0.019 | 0.273 | 0.021 | 0.029 | 1.86 | Balloon will burst if used w／rec．fill | 0.0043 | 0.0022 | －7．86 | －7．84 | 2.771 | 9.724 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 17 | 0.022 | 0.318 | 0.024 | 0.034 | 1.59 | Balloon will burst if used w／rec．fill | 0.0050 | 0.0025 | －7．86 | －7．84 | 2.630 | 9.727 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 18 | 0.025 | 0.370 | 0.029 | 0.040 | 1.36 | Balloon will burst if used w／rec．fill | 0.0059 | 0.0029 | －7．86 | －7．84 | 2.496 | 9.730 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 19 | 0.029 | 0.431 | 0.034 | 0.047 | 1.16 | Balloon will burst if used w／rec．fill | 0.0069 | 0.0035 | －7．86 | －7．84 | 2.368 | 9.733 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 20 | 0.034 | 0.503 | 0.039 | 0.055 | 0.99 | Balloon will burst if used w／rec．fill | 0.0080 | 0.0040 | －7．86 | －7．85 | 2.246 | 9.736 | 0.047 | 0.051 | 0.453 | 0.492 |  |
| 21 | 0.040 | 0.588 | 0.046 | 0.065 | 0.84 | Balloon will burst if used w／rec．fill | 0.0094 | 0.0048 | －7．86 | －7．85 | 2.131 | 9.742 | 0.047 | 0.050 | 0.453 | 0.492 |  |
| 22 | 0.047 | 0.686 | 0.054 | 0.076 | 0.72 | Balloon will burst if used w／rec．fill | 0.0111 | 0.0056 | －7．86 | －7．85 | 2.019 | 9.742 | 0.047 | 0.050 | 0.453 | 0.492 |  |
| 23 | 0.055 | 0.803 | 0.064 | 0.089 | 0.61 | Balloon will burst if used w／rec．fill | 0.0130 | 0.0066 | －7．86 | －7．85 | 1.914 | 9.745 | 0.047 | 0.050 | 0.453 | 0.492 |  |
| 24 | 0.064 | 0.939 | 0.074 | 0.104 | 0.52 | Balloon will burst if used w／rec．fill | 0.0152 | 0.0077 | －7．86 | －7．85 | 1.817 | 9.748 | 0.047 | 0.050 | 0.453 | 0.492 |  |
| 25 | 0.075 | 1.098 | 0.087 | 0.122 | 0.45 | Balloon will burst if used w／rec．fill | 0.0178 | 0.0090 | －7．86 | －7．85 | 1.725 | 9.751 | 0.047 | 0.050 | 0.454 | 0.492 |  |
| 26 | 0.087 | 1.284 | 0.102 | 0.142 | 0.38 | Balloon will burst if used w／rec．fill | 0.0208 | 0.0105 | －7．86 | －7．85 | 1.638 | 9.754 | 0.047 | 0.050 | 0.454 | 0.492 |  |
| 27 | 0.102 | 1.503 | 0.119 | 0.166 | 0.33 | Balloon will burst if used w／rec．fill | 0.0244 | 0.0123 | －7．86 | －7．85 | 1.555 | 9.758 | 0.047 | 0.050 | 0.454 | 0.492 |  |
| 28 | 0.120 | 1.758 | 0.139 | 0.195 | 0.28 | Balloon will burst if used w／rec．fill | 0.0285 | 0.0143 | －7．85 | －7．85 | 1.476 | 9.761 | 0.047 | 0.050 | 0.454 | 0.493 |  |
| 29 | 0.140 | 2.056 | 0.162 | 0.228 | 0.24 | Balloon will burst if used w／rec．fill | 0.0332 | 0.0167 | －7．82 | －7．82 | 1.409 | 9.764 | 0.047 | 0.051 | 0.457 | 0.495 |  |
| 30 | 0.164 | 2.406 | 0.189 | 0.267 | 0.21 | Balloon will burst if used w／rec．fill | 0.0386 | 0.0195 | －7．78 | －7．78 | 1.345 | 9.767 | 0.047 | 0.051 | 0.459 | 0.498 |  |
| 14 | なカに | Ascent Ch | （non－Rec． | Fil）Des | scent Calcula | ations（SB）Descent Data T | Descent Cha | arts（SB）De | escent（i） 4 |  |  |  | ｜II |  |  |  |  |

## Database: Descent with Small Balloon

- Descent Charts (SB) Worksheet

Volume of Decent Balloon with Altitude

$R^{2}=0.9965$

## Database: Descent with Parachute

- Descent Calculations (Parachute) Worksheet



## Database: Descent with Parachute

- Descent Data Table (Parachute) Worksheet

| 1 | A | B | C | D | E | F | G | H | I | $J$ | K | L | M | N |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Altitude | Altitude | Time | Temp. Atmo. | Temp. Atmo. | Pressure | Pressure | $\rho$ of air | V Down | Coef. of Drag | Gravity | Drag Force w/ $\mathrm{m}_{\text {tot }}$ |  | Troposphere |
| 2 | (km) | (ft) | (s) | (K) | $\left({ }^{\circ} \mathrm{C}\right)$ | (atm) | (Psi) | (kg/m) | ( $\mathrm{m} / \mathrm{s}$ ) | Cd | $\left(\mathrm{m} / \mathrm{s}^{2}\right)$ | (N) |  | temp decrease with altitude increase |
| 3 | 40 | 131200 | 0 | 250.35 | -22.80 | 0.003 | 0.042 | 0.004 | 64.04 | 1.50 | 9.684 | 20.34 |  | Tropopause |
| 4 | 39 | 127920 | 17 | 247.58 | -25.57 | 0.003 | 0.048 | 0.005 | 59.52 | 1.50 | 9.687 | 20.34 |  | temp constant with altitude increase |
| 5 | 38 | 124640 | 35 | 244.82 | -28.33 | 0.004 | 0.055 | 0.005 | 55.28 | 1.50 | 9.690 | 20.35 |  | Upper Stratosphere |
| 6 | 37 | 121360 | 54 | 242.05 | -31.10 | 0.004 | 0.063 | 0.006 | 51.29 | 1.50 | 9.694 | 20.36 |  | temp increase with altitude increase |
| 7 | 36 | 118080 | 75 | 239.28 | -33.87 | 0.005 | 0.072 | 0.007 | 47.55 | 1.50 | 9.697 | 20.36 |  | Additional comment |
| 8 | 35 | 114800 | 98 | 236.51 | -36.64 | 0.006 | 0.083 | 0.008 | 44.04 | 1.50 | 9.700 | 20.37 |  | reletivily un-experimented space |
| 9 | 34 | 111520 | 123 | 233.74 | -39.41 | 0.007 | 0.096 | 0.010 | 40.75 | 1.50 | 9.703 | 20.38 |  |  |
| 10 | 33 | 108240 | 149 | 230.97 | -42.18 | 0.008 | 0.111 | 0.012 | 37.67 | 1.50 | 9.706 | 20.38 |  |  |
| 11 | 32 | 104960 | 178 | 228.49 | -44.66 | 0.009 | 0.129 | 0.014 | 34.81 | 1.50 | 9.709 | 20.39 |  |  |
| 12 | 31 | 101680 | 209 | 227.50 | -45.65 | 0.010 | 0.150 | 0.016 | 32.26 | 1.50 | 9.712 | 20.39 |  |  |
| 13 | 30 | 98400 | 242 | 226.51 | -46.64 | 0.012 | 0.174 | 0.018 | 29.88 | 1.50 | 9.715 | 20.40 |  |  |
| 14 | 29 | 95120 | 279 | 225.52 | -47.63 | 0.014 | 0.202 | 0.021 | 27.67 | 1.50 | 9.718 | 20.41 |  |  |
| 15 | 28 | 91840 | 318 | 224.53 | -48.62 | 0.016 | 0.235 | 0.025 | 25.61 | 1.50 | 9.721 | 20.41 |  |  |
| 16 | 27 | 88560 | 360 | 223.54 | -49.61 | 0.019 | 0.273 | 0.029 | 23.70 | 1.50 | 9.724 | 20.42 |  |  |
| 17 | 26 | 85280 | 405 | 222.54 | -50.61 | 0.022 | 0.318 | 0.034 | 21.92 | 1.50 | 9.727 | 20.43 |  |  |
| 18 | 25 | 82000 | 455 | 221.55 | -51.60 | 0.025 | 0.370 | 0.040 | 20.27 | 1.50 | 9.730 | 20.43 |  |  |
| 19 | 24 | 78720 | 508 | 220.56 | -52.59 | 0.029 | 0.431 | 0.047 | 18.73 | 1.50 | 9.733 | 20.44 |  |  |
| 20 | 23 | 75440 | 566 | 219.57 | -53.58 | 0.034 | 0.503 | 0.055 | 17.31 | 1.50 | 9.736 | 20.45 |  |  |
| 21 | 22 | 72160 | 628 | 218.57 | -54.58 | 0.040 | 0.588 | 0.065 | 15.99 | 1.50 | 9.742 | 20.46 |  |  |
| 22 | 21 | 68880 | 696 | 217.58 | -55.57 | 0.047 | 0.686 | 0.076 | 14.76 | 1.50 | 9.742 | 20.46 |  |  |
| 23 | 20 | 65600 | 770 | 216.65 | -56.50 | 0.055 | 0.803 | 0.089 | 13.62 | 1.50 | 9.745 | 20.46 |  |  |
| 24 | 19 | 62320 | 849 | 216.65 | -56.50 | 0.064 | 0.939 | 0.104 | 12.59 | 1.50 | 9.748 | 20.47 |  |  |
| 25 | 18 | 59040 | 935 | 216.65 | -56.50 | 0.075 | 1.098 | 0.122 | 11.65 | 1.50 | 9.751 | 20.48 |  |  |
| 26 | 17 | 55760 | 1028 | 216.65 | -56.50 | 0.087 | 1.284 | 0.142 | 10.77 | 1.50 | 9.754 | 20.48 |  |  |
| 27 | - 16 | $52480$ | 1128 | 21ヶ65 | -56.50 | 0102 | 1502 | 0166 | 9.96 | 150 | 9758 | 20.49 |  |  |
| 14. | -ハ D | escent Charts | (SB) De | escent Calc. (Para | chute) Descen | nt Data Tab | le (Parachut | te) Desce | ent Charts (P | arachute) E0 | 214 |  |  | 1 |

## Database: Descent with Parachute

- Descent Charts (Parachute) Worksheet



## Additional Notes and Future Work

- Acceleration?
- Coefficient of Drag
- Drag Force, Lifting Force, and Free Lift
- Ideas for Possible Database Additions
- Beta Test
- Website:
- http://cse.taylor.edu/~nramm/High_Altitude_Balloon_Databases/


## Conclusions

- More Fill
- Doesn't Give a Higher Altitude
- Faster Ascent Rate
- Ending Thoughts


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